

Hello ST,

I am a NEW hire in our company and I am trying to understand the Analog PFC in our current design using L4981A PFC controller IC.

I need to fully understand the feedback control portion in this circuit because we are having some input current oscillation problems (Dancing waveform that is non-sinusoidal).

I am referring to the L4981A's application note for help. You can access it in this link:

http://www.st.com/content/ccc/resource/technical/document/application_note/94/6e/ec/8c/4c/3e/40/a9/CD00003936.pdf/files/CD00003936.pdf/jcr:content/translations/en.CD00003936.pdf

We have plans to move into TI products especially the UCD3138A IC family of digital PFC solutions.

My questions below are related to how to select compensation network values for the inner current loop of Boost PFC.

Doubts from pages 7,8 & 9

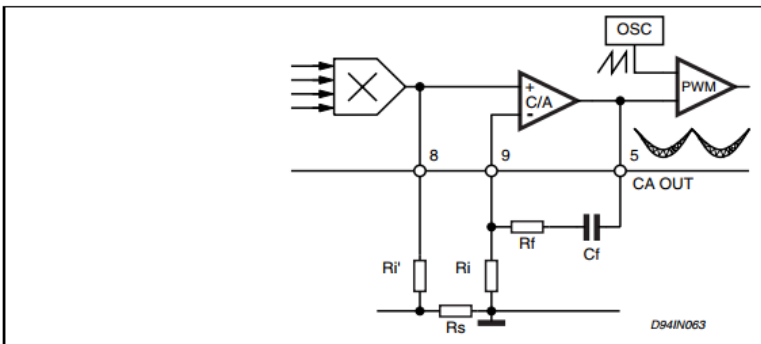
The equation below is trying to say that the inductor down slope must be smaller than the ramp up slope of the PWM ramp that sets the switching frequency.

Inductor ramp down slope (we are seeing from negative side of sense resistor, before GND) is during Boost MOSFET turn ON so the voltage across inductor should be V_{in} and NOT V_O like it is shown in the equation below right?

$$\frac{V_O}{L} \cdot R_s \cdot G_{ca} \leq V_{srp} \cdot f_{sw}$$

What is the value of the current amplifier gain? Is it made up of low frequency gain and high frequency gain referring to figure 9.

Figure 9.



Actually the multiplication, $(V_O/L \cdot R_s \cdot G_{ca})$ is the quantity of gradient that is output from C/A right?

From page 9.

How is the voltage V_{rs} equal to below? I do not understand how V_{rs} is found by taking the input voltage (gradient), V_{rs} of +ve terminal of C/A and multiplying it to $1/S$?

Because, in worst condition is:

$$v_{rs} = \frac{R_s \cdot V_O}{s \cdot L}$$

What is the meaning of worst condition here? where did this integrator with DC pole come from?

What is the quantity G_{avg} ?

How did G_{avg} come to be as shown below? What is its physical meaning?

$$G_{avg} = \frac{R_s \cdot V_O}{V_{srp} \cdot 2\pi \cdot f \cdot L}$$

Why is G_{avg} multiplied to G_{ca} ? Are they combining two transfer functions? Is G_{ca} the high frequency transfer function or G_{avg} ? What is the reason to split them?

Multiplying this G_{avg} by G_{ca} and solving for the crossover frequency ($f = f_c$), follows:

$$f_c = \frac{f_{sw}}{2\pi}$$

The crossover frequency comes to the above after I equated $G_{ca} \cdot G_{avg} = 0'$

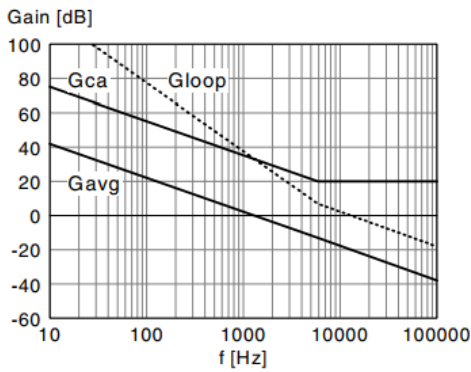
Where did the zero come from in the below equation? G_{ca} is not frequency dependent and G_{avg} only has an integrator with DC pole so where did the zero come from?

To ensure a phase margin (higher than 45°), the zero frequency (f_z) should be about $\frac{f_c}{2}$, than:

$$f_z = \frac{f_{sw}}{4 \cdot \pi} = \frac{1}{2 \cdot \pi \cdot C_f \cdot R_f} \Rightarrow C_f = \frac{2}{R_f \cdot f_{sw}}$$

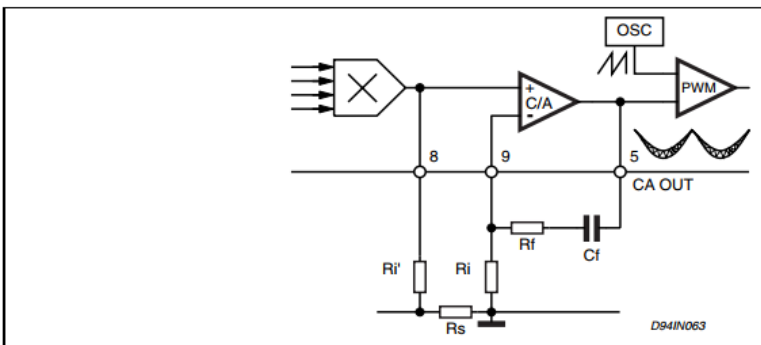
Also why is there a zero in G_{ca} around 6000 Hz in the below graph? Where did it come from?

Figure 11.



Please also give the closed loop final transfer function of the compensation network shown in Figure 9

Figure 9.



Please help to answer my questions as I try to understand the current loop compensation portion of this PFC boost converter.

Thank you for your help.

Regards,

Peeterson.